

# Brinicles of Death!

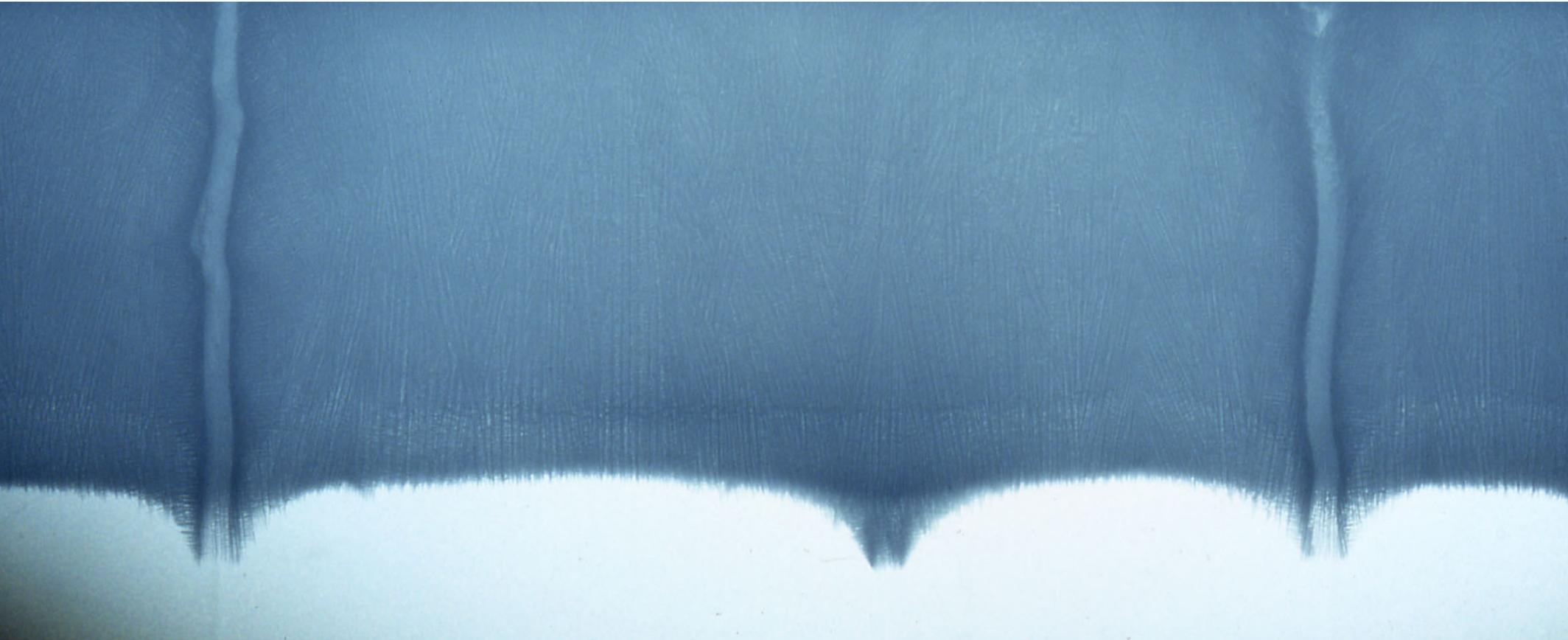


BBC Frozen Planet 2011

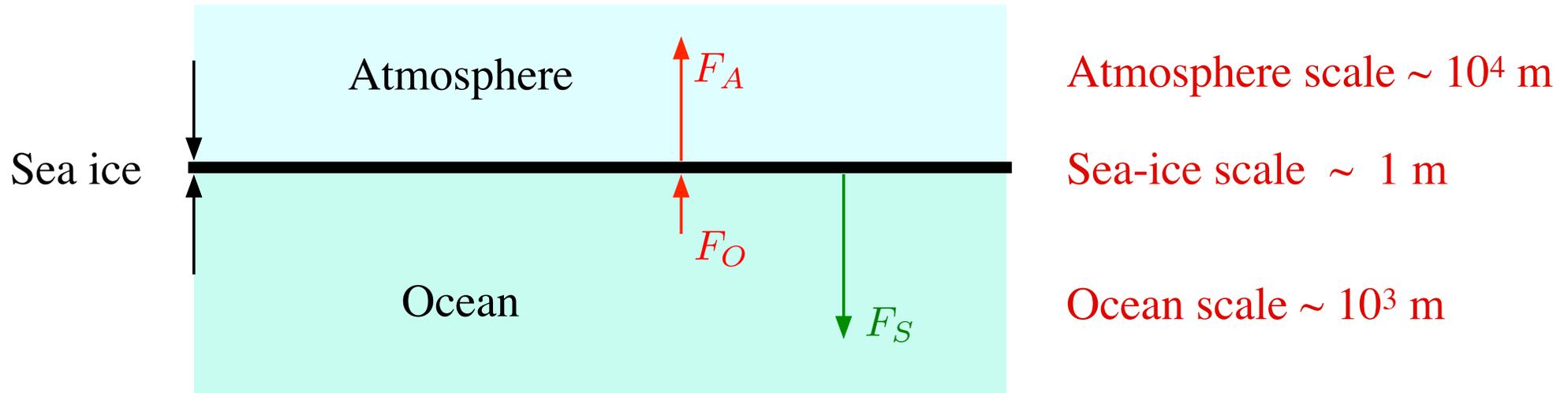
# Brine Drainage from Sea Ice

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## Sea Ice as an Interface



Simplest thermodynamic model

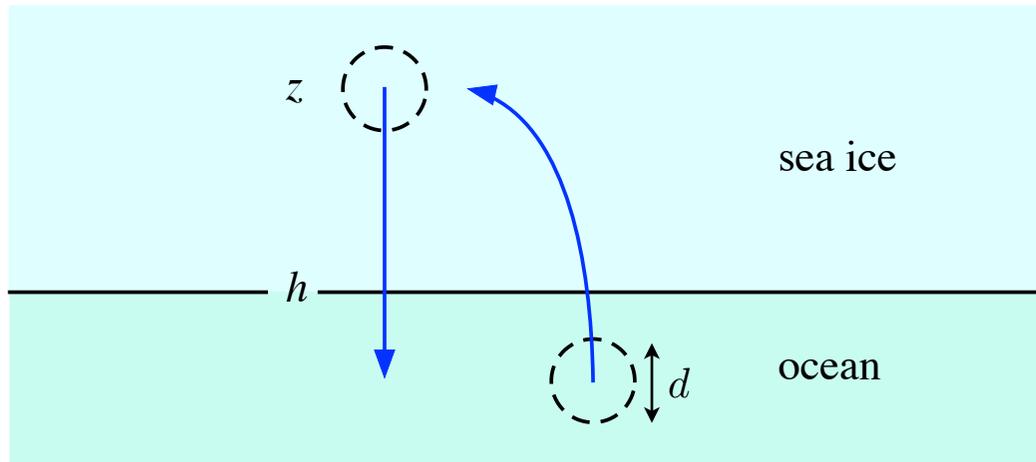
$$\rho L \phi \frac{dh}{dt} = F_A - F_O = k(\phi) \frac{T_O - T_A}{h} - F_O$$

is one-dimensional

# Brine Drainage from Sea Ice



# Fundamentals of Convection in Mushy Layers



Potential energy released  $PE \sim \rho_0 \beta [S_{br}(z) - S_0] d^3 g (h - z)$

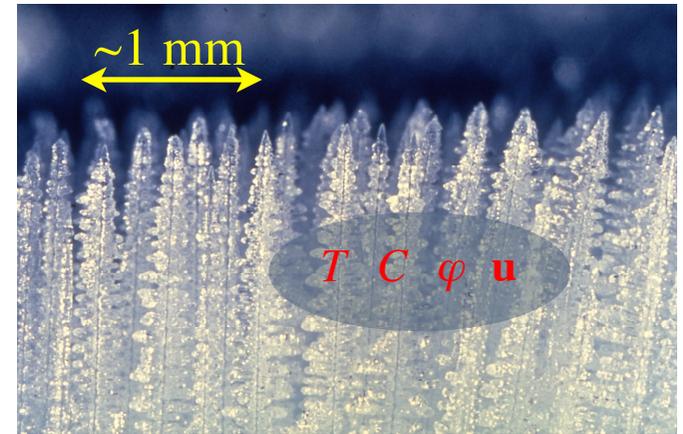
Dissipation  $D \sim \Delta p d^2 (h - z) \sim \frac{\mu U}{\Pi} (h - z) d^2 (h - z)$

Parcel runs out of buoyancy if  $\tau \sim \frac{h}{U} \gtrsim \frac{d^2}{\kappa}$

Optimal conversion of potential energy into kinetic energy (convection) if

$$\tau \sim \frac{d^2}{\kappa} \quad \text{and} \quad d \sim h - z \quad \Rightarrow \quad R_m \equiv \frac{\beta [S_{br} - S_0] g (h - z) \Pi}{\kappa U} \gtrsim 1$$

# Convection in a Mushy Layer (Sea Ice)



Conservation of heat

$$\frac{\partial T}{\partial t} + \mathbf{u} \cdot \nabla T = \kappa \nabla^2 T + \frac{L}{c_p} \frac{\partial \phi}{\partial t}$$

Conservation of salt

$$(1 - \phi) \frac{\partial C}{\partial t} + \mathbf{u} \cdot \nabla C = C \frac{\partial \phi}{\partial t} \quad \text{ignore diffusion of salt}$$

Liquidus constraint

$$T = T_m - mC$$

Darcy's equation  
for flow in a porous medium

$$\mu \mathbf{u} = \Pi [-\nabla p + \rho \mathbf{g}]$$

Incompressibility

$$\nabla \cdot \mathbf{u} = 0$$

Constitutive relation

$$\rho = \rho_0 [1 + \beta(C - C_0)]$$

# Scaling

Suppose that system is solidifying at rate  $V$  and scale

velocities with  $V$    lengths with  $\kappa/V$    time with  $\kappa/V^2$    pressure with  $\Delta\rho g\kappa/V$

Write  $\theta = \frac{T - T_0}{\Delta T} = -\frac{C - C_0}{\Delta C}$    where  $\Delta T = m\Delta C$

$$\begin{aligned} \frac{\partial\theta}{\partial t} + \mathbf{u} \cdot \nabla\theta &= \nabla^2\theta + \mathcal{S} \frac{\partial\phi}{\partial t} & \Omega \frac{D\theta}{Dt} &= \nabla^2\theta \\ (1 - \phi) \frac{\partial\theta}{\partial t} + \mathbf{u} \cdot \nabla\theta &= (\theta - \mathcal{C}) \frac{\partial\phi}{\partial t} & \frac{\partial\phi}{\partial t} &= -\frac{1}{\mathcal{C}} \frac{D\theta}{Dt} \\ \mathbf{u} &= R_m [-\nabla p + \theta\mathbf{k}] & \mathbf{u} &= R_m [-\nabla p + \theta\mathbf{k}] \end{aligned}$$

$$\begin{aligned} \mathcal{S} \gg 1, \quad \mathcal{C} \gg 1 \\ \xrightarrow{\hspace{1cm}} \\ \frac{\mathcal{S}}{\mathcal{C}} = O(1) \end{aligned}$$

$$\nabla \cdot \mathbf{u} = 0$$

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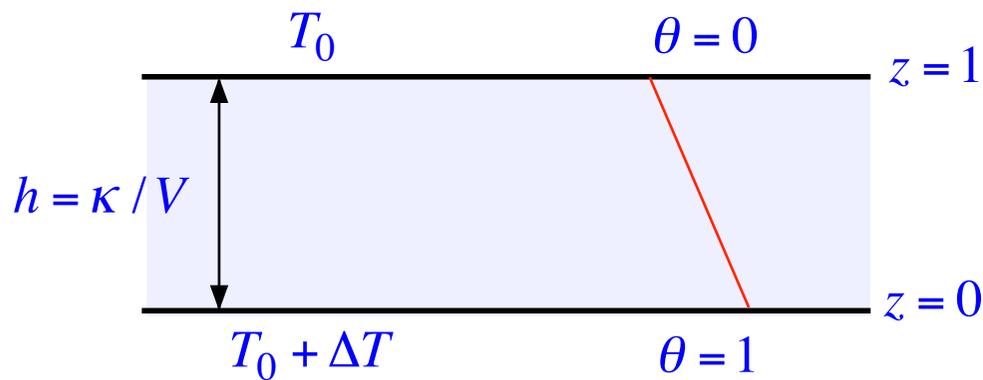
$$\mathcal{S} = \frac{L}{c_p \Delta T}$$

$$\mathcal{C} = \frac{C_0}{\Delta C}$$

$$\Omega = 1 + \frac{\mathcal{S}}{\mathcal{C}}$$

$$R_m = \frac{\beta \Delta C g \Pi(\kappa/V)}{\kappa V}$$

# Indicative Stability Analysis



$$\Omega \left( \frac{\partial \theta}{\partial t} + \mathbf{u} \cdot \nabla \theta \right) = \nabla^2 \theta$$

$$\mathbf{u} = R_m [-\nabla p + \theta \mathbf{k}]$$

$$\nabla \cdot \mathbf{u} = 0$$

Write  $\mathbf{u} = (u, w)$

$$\theta = 1 - z + \hat{\theta}(z) e^{i\alpha x + \sigma t}$$

$$w = \hat{w}(z) e^{i\alpha x + \sigma t}$$

Substitute, linearize and look for marginal (steady) states with  $\sigma = 0$

$$D \equiv \frac{d}{dz}$$

$$-\Omega \hat{w} = (D^2 - \alpha^2) \hat{\theta}$$

$$(D^2 - \alpha^2) \hat{w} = \alpha^2 R_m \hat{\theta}$$

$\Rightarrow$

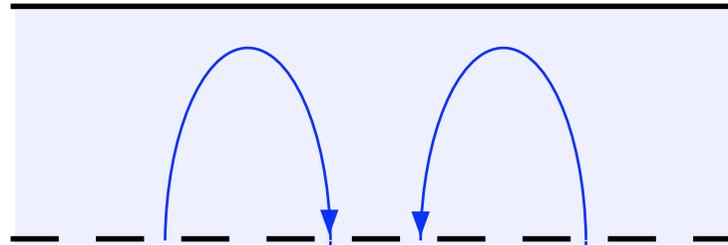
$$(D^2 - \alpha^2)^2 \hat{w} = -\alpha^2 \Omega R_m \hat{w}$$

# Marginal Stability Results

$$(D^2 - \alpha^2)^2 \hat{w} = -\alpha^2 \Omega R_m \hat{w}$$

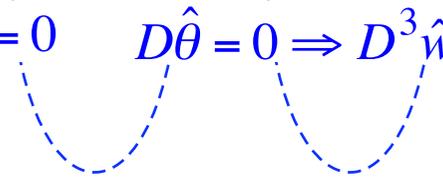
No flow, constant temperature

$$\hat{w} = 0 \quad \hat{\theta} = 0 \Rightarrow D^2 \hat{w} = 0$$



Constant pressure and heat flux

$$D\hat{w} = 0 \quad D\hat{\theta} = 0 \Rightarrow D^3 \hat{w} = 0$$



$$\hat{w} \propto \sin\left[\left(n + \frac{1}{2}\right)\pi(1 - z)\right] \quad \Omega R_m = \frac{\left[\left(n + \frac{1}{2}\right)^2 \pi^2 + \alpha^2\right]^2}{\alpha^2}$$

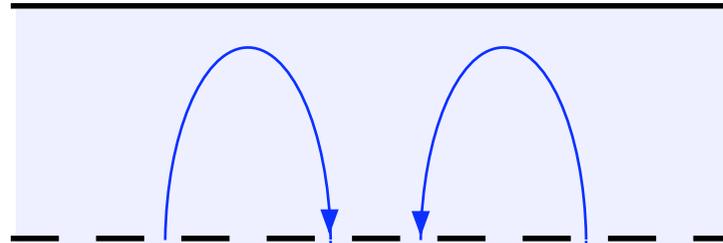
Lowest (most unstable) mode has  $n=0$

$$\Omega R_m = \frac{\left[\frac{\pi^2}{4} + \alpha^2\right]^2}{\alpha^2}$$

# Marginal Stability Results

No flow, constant temperature

$$\hat{w} = 0 \quad \hat{\theta} = 0$$



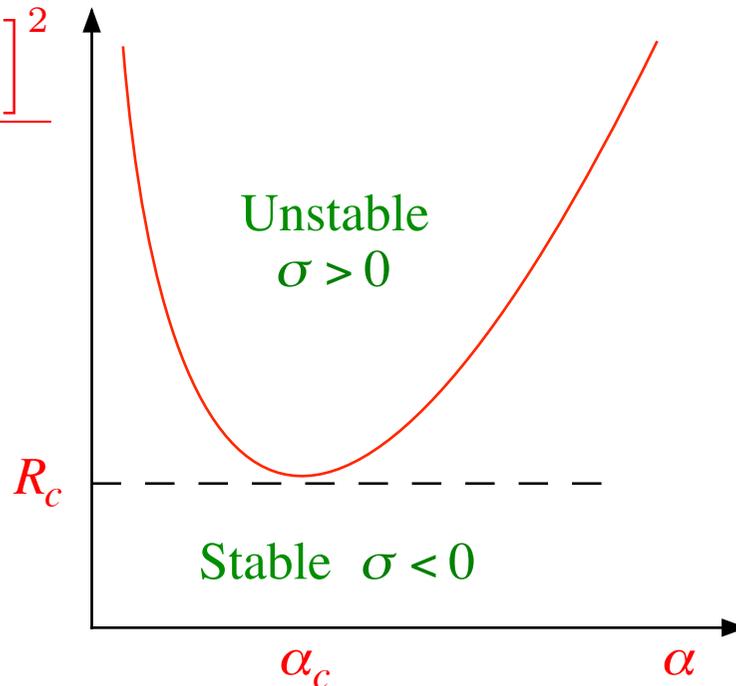
$$\theta = 1 - z + \hat{\theta}(z)e^{i\alpha x + \sigma t}$$

$$w = \hat{w}(z)e^{i\alpha x + \sigma t}$$

Constant pressure and heat flux

$$D\hat{w} = 0 \quad D\hat{\theta} = 0$$

$$\Omega R_m = \frac{\left[\frac{\pi^2}{4} + \alpha^2\right]^2}{\alpha^2}$$

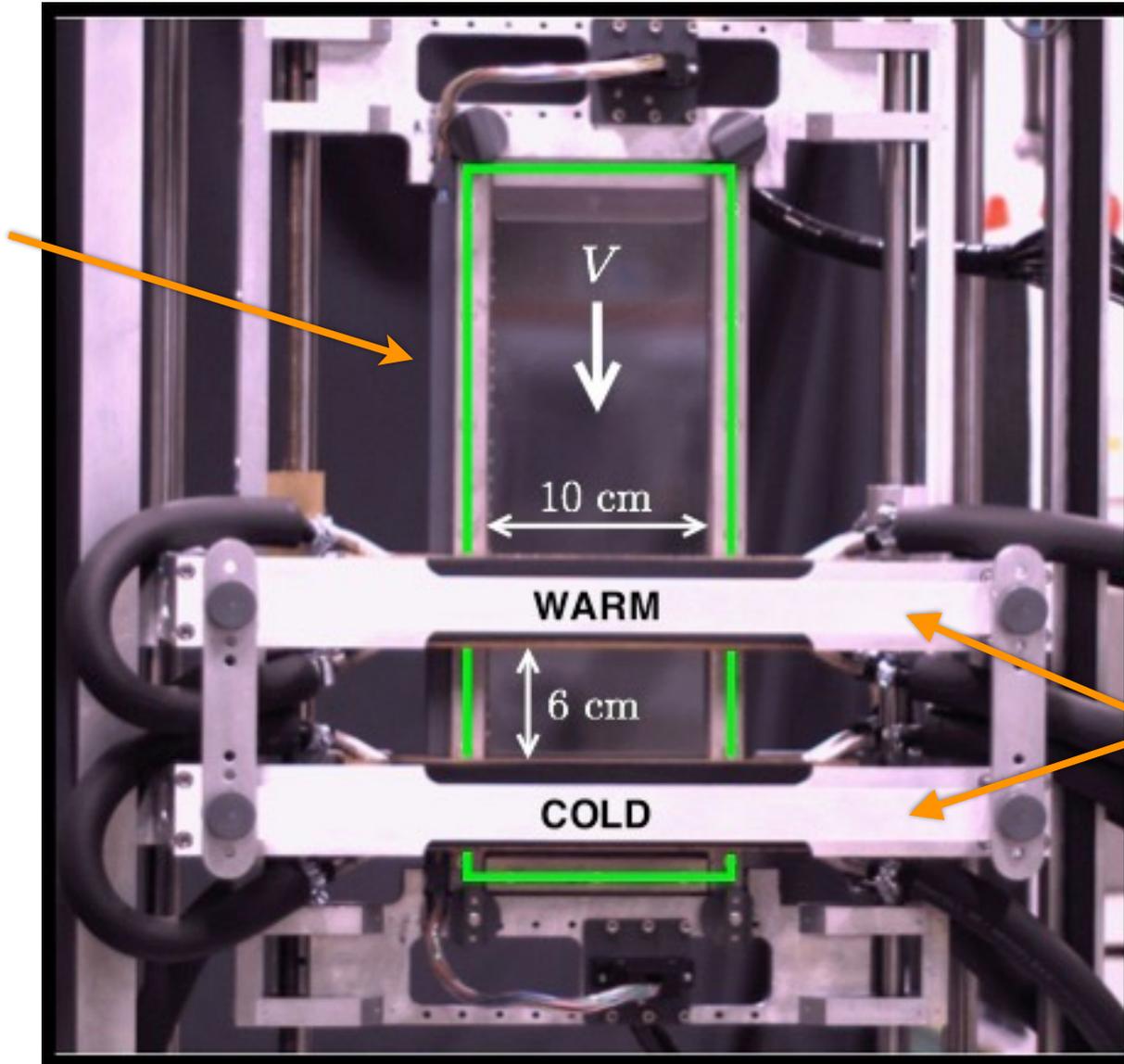


Instability if

$$\Omega R_m > R_c = \pi^2 \approx 10$$

# Directional Solidification

(3 mm gap)

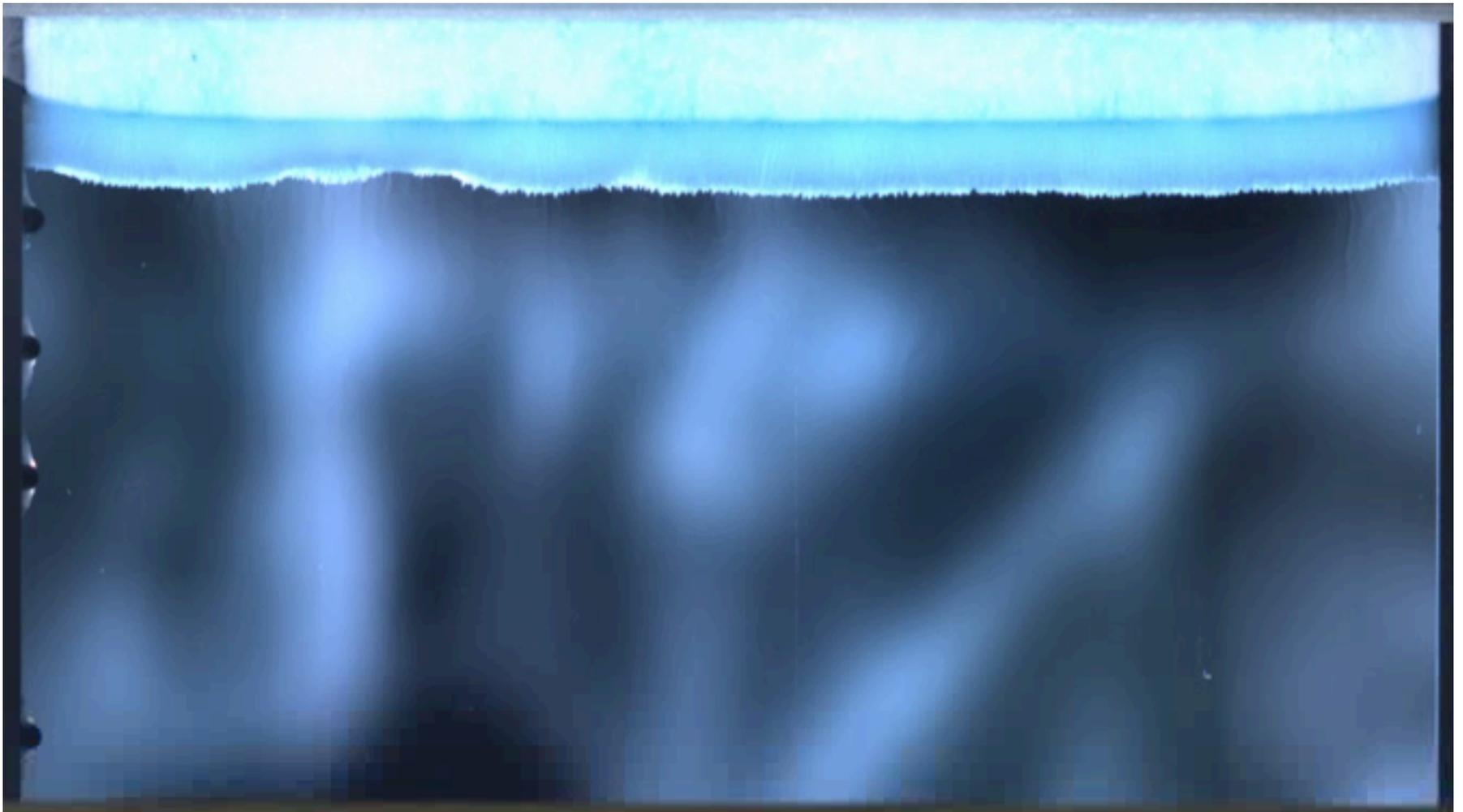


Fixed-temperature  
heat exchangers

## Dynamic Control of Brine Rejection

$$R_m = \frac{\beta \Delta C g \Pi (\kappa/V)}{\kappa \nu}$$

$$V = 2 \mu\text{m s}^{-1} \rightarrow 0.5 \mu\text{m s}^{-1} \rightarrow 2 \mu\text{m s}^{-1}$$

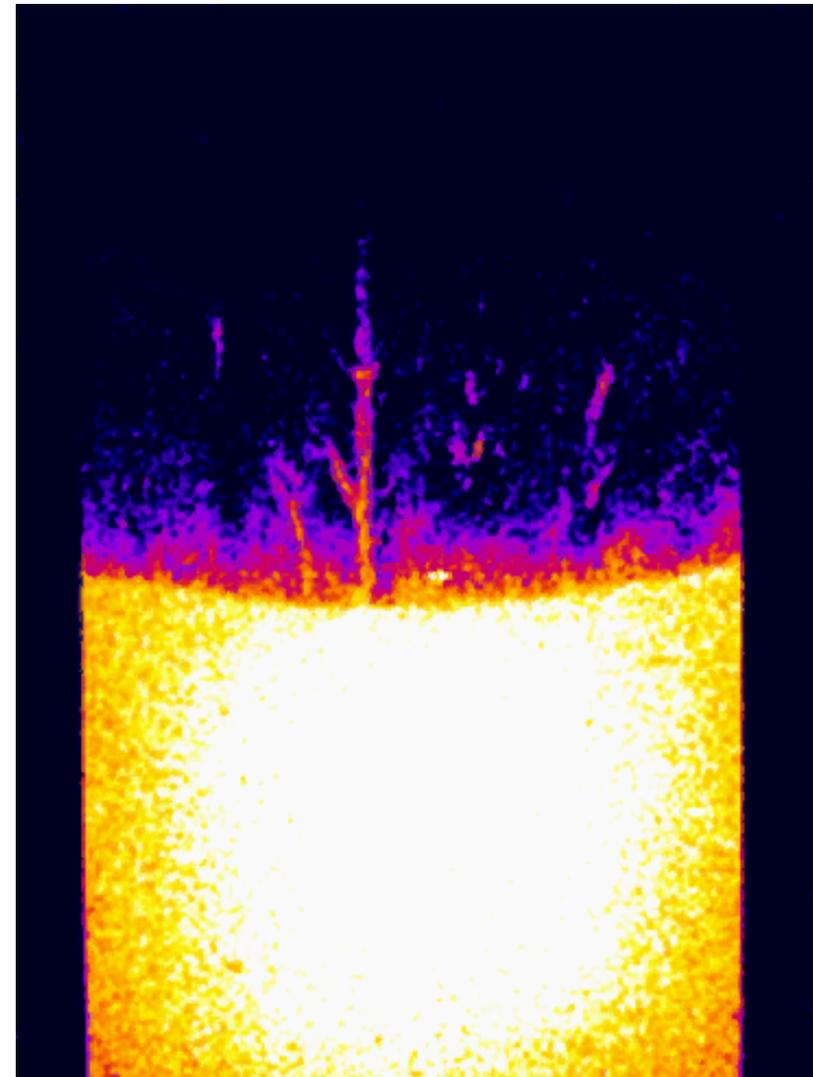
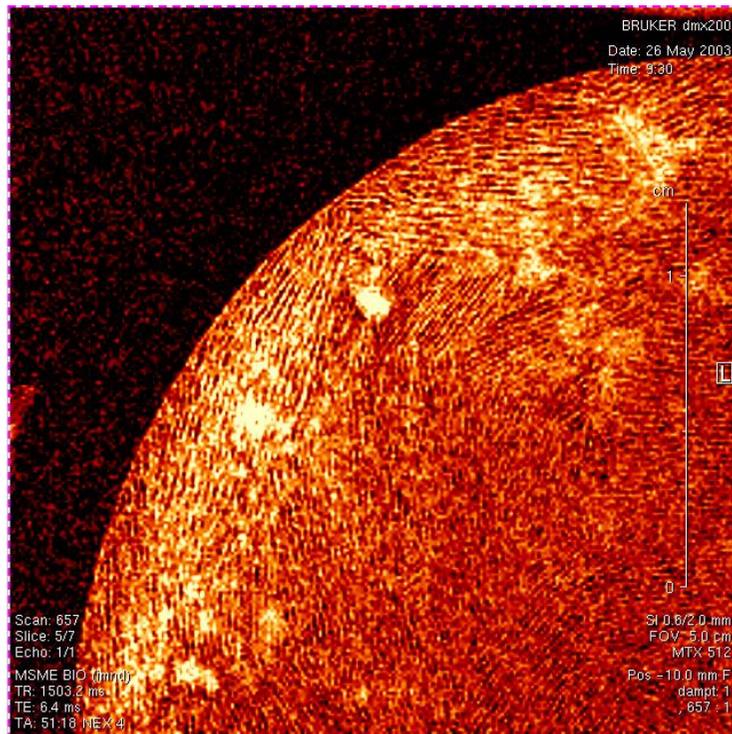


# MRI study of structure and flow in convecting sea ice

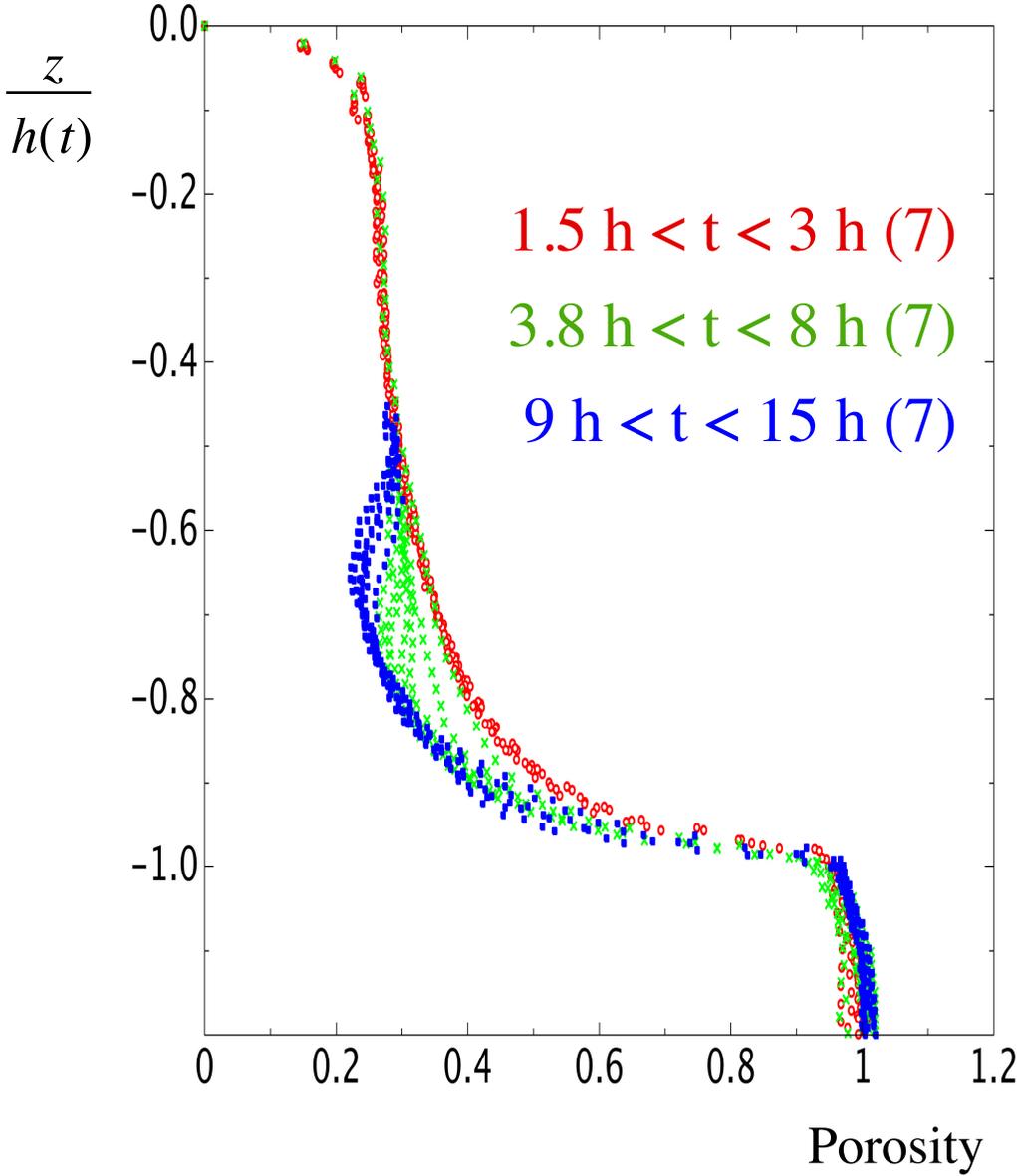
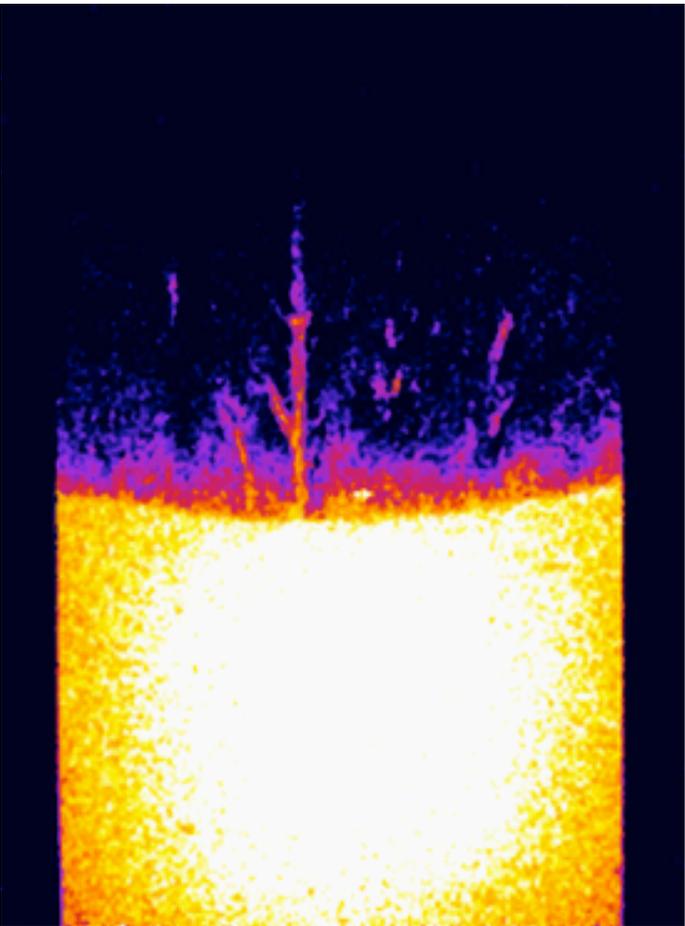
Aussillous, Sederman, Gladden, Huppert & Worster

Vertical cross-section through  
an evolving brine channel

Horizontal cross-section of  
platelets and brine channels



# Evolution of Solid Fraction



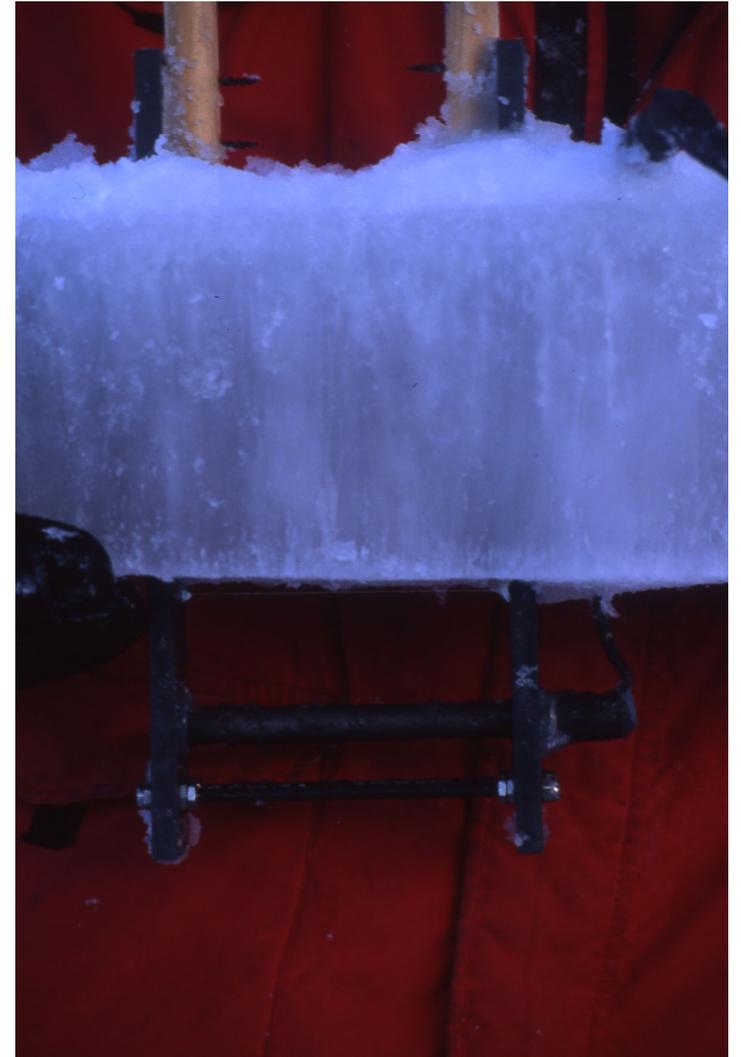
# Van Mijen Fjord, Svalbard 2001



# Field Experiments



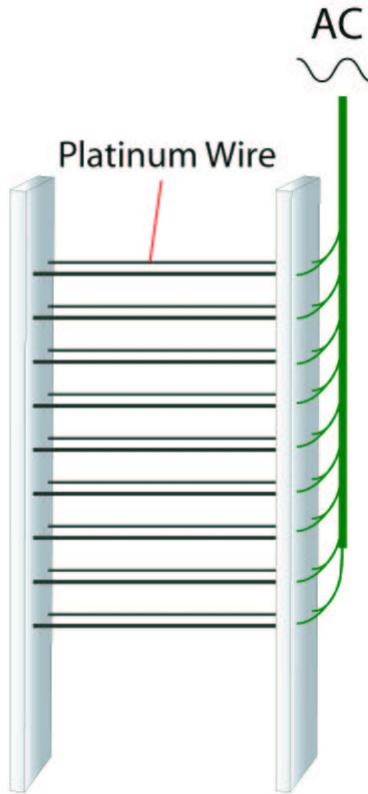
John Wettlaufer



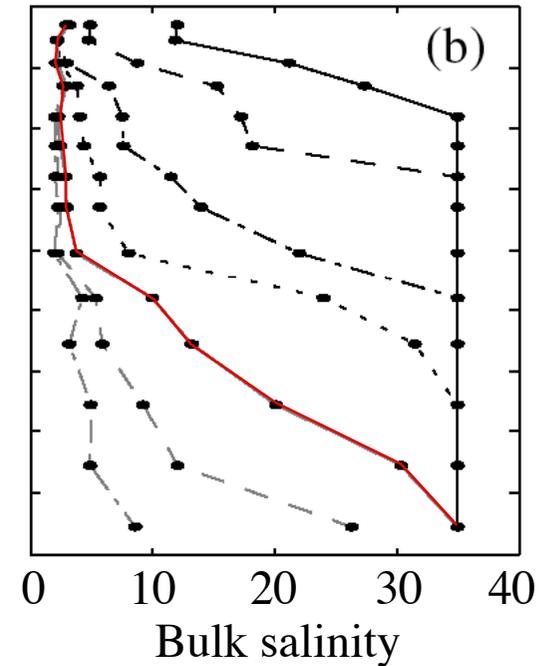
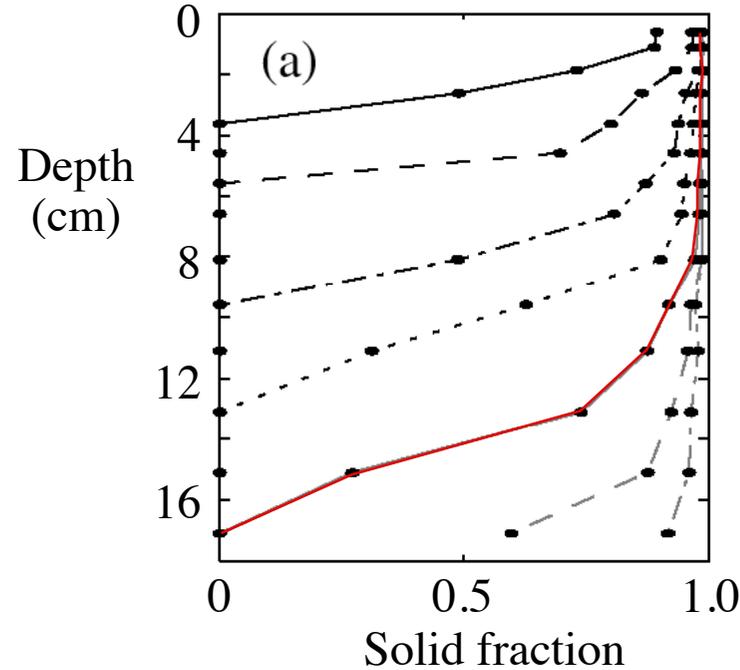
Dirk Notz

# Field Measurements of Porosity and Salinity

Notz, Wettlaufer & Worster



## Impedance measurement of solid fraction

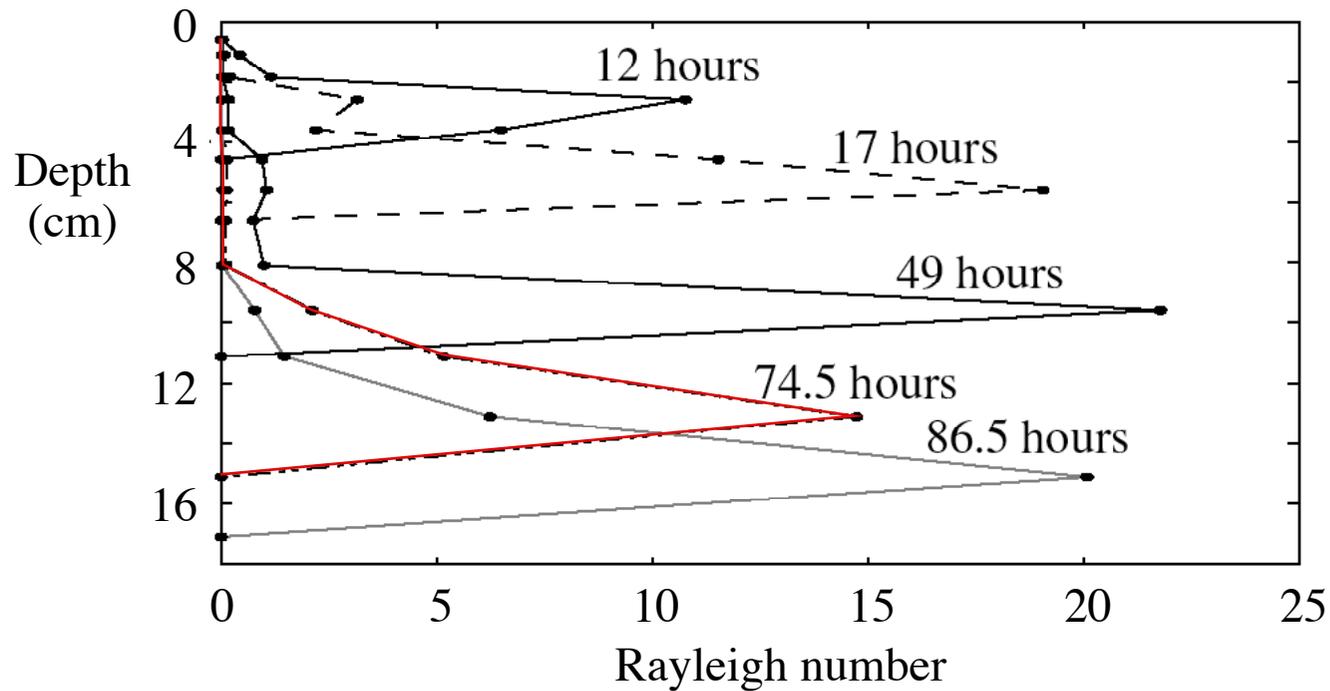


$$(1 - \phi) \propto \text{conductance}$$

$$C_B = (1 - \phi) \left( \frac{T_m - T}{m} \right)$$

# Derived Measurements of Local Rayleigh Number

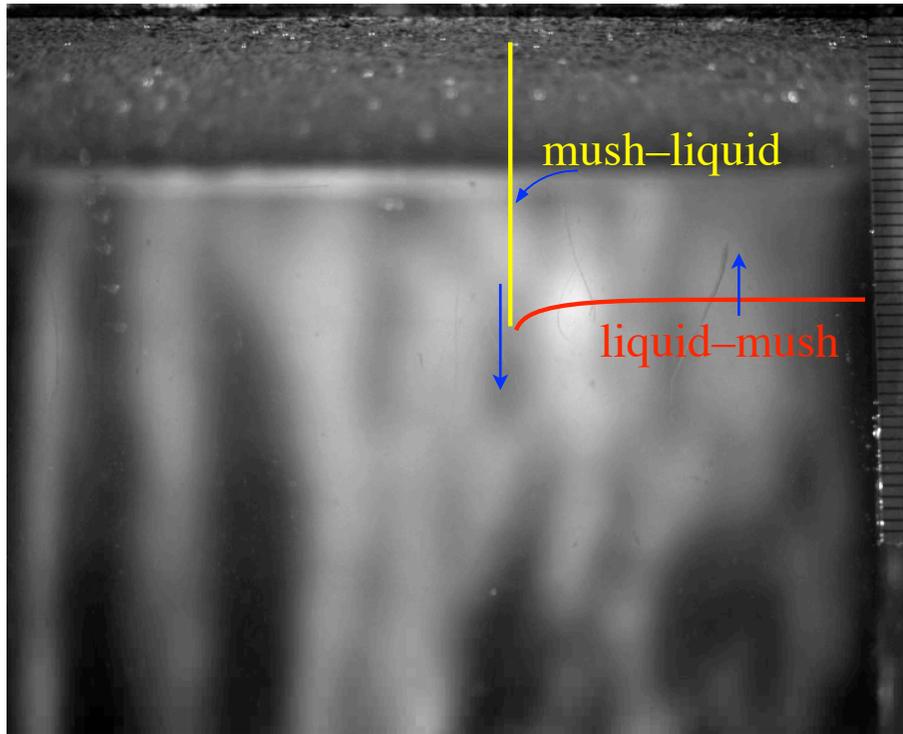
$$R_m = \frac{\beta g [C(z) - C_0] \Pi(z) h}{\kappa \nu}$$



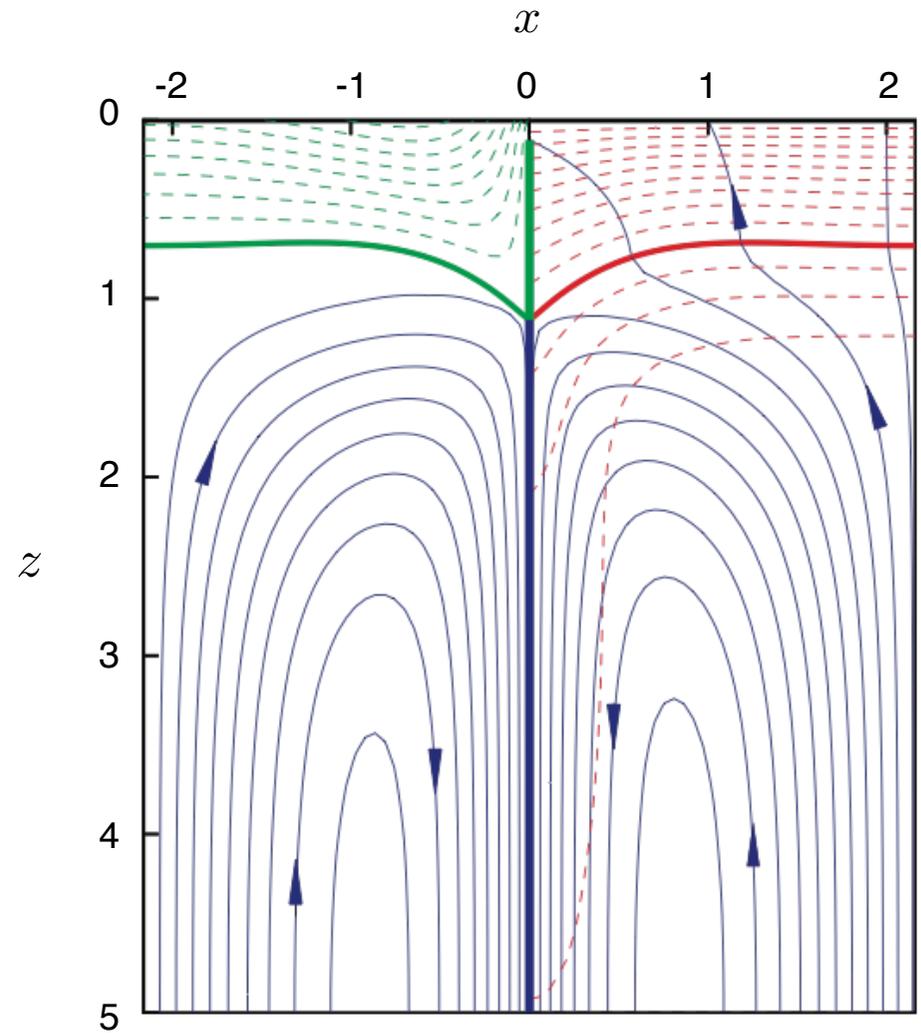
# 2D Numerical Modelling

$$\frac{\partial \phi}{\partial t} = -\frac{1}{c} \frac{D\theta}{Dt}$$

Cold

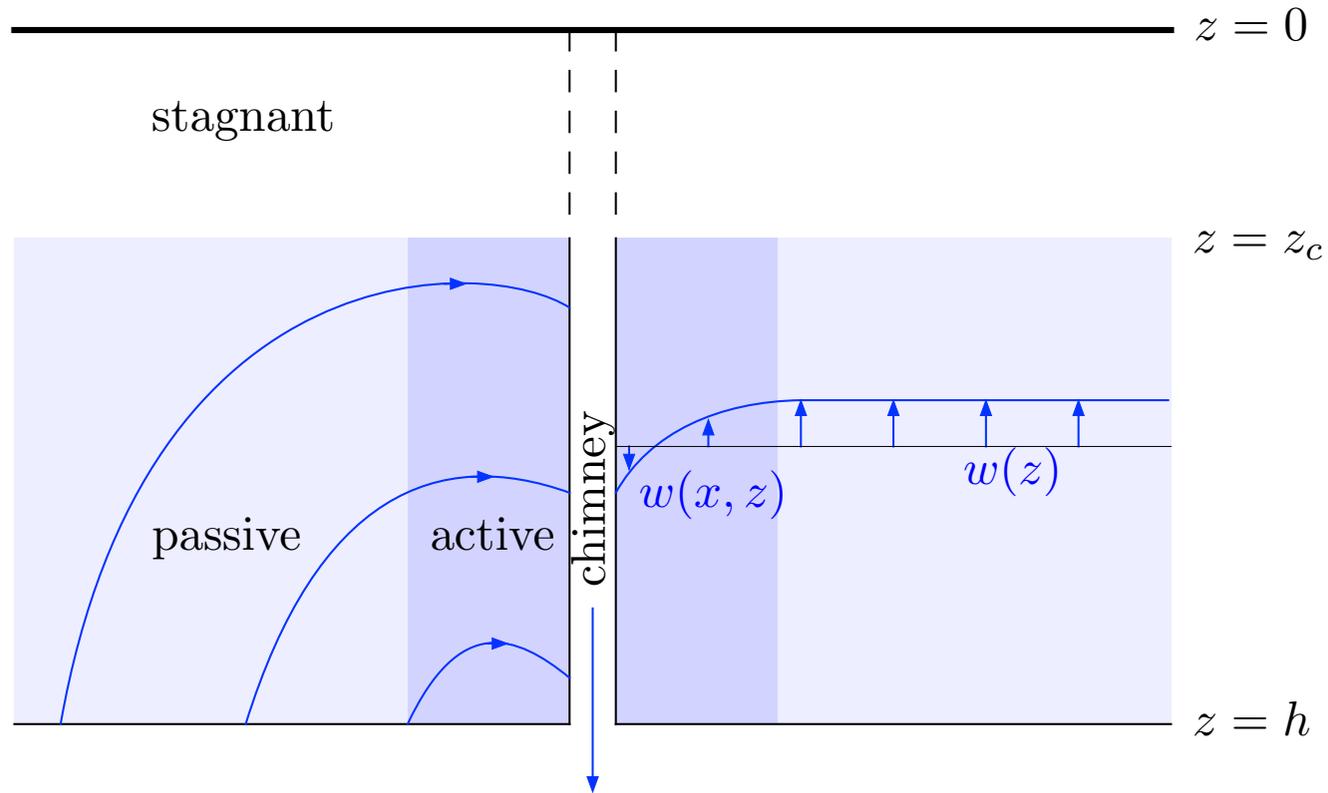


Warm



# CAP Model of Convection with Brine Channels

Rees Jones & Worster

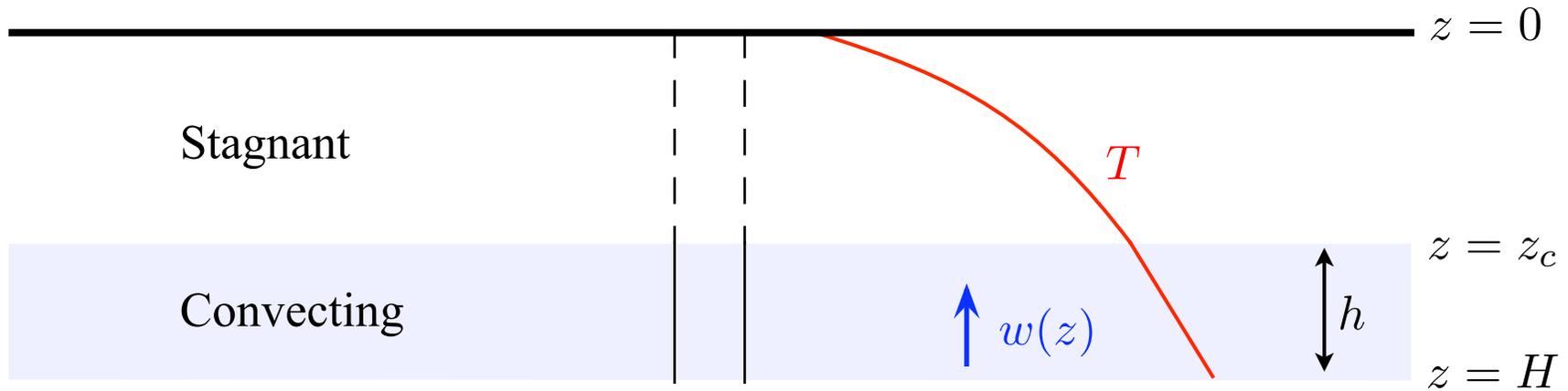


Determine channel spacing by optimising the buoyancy flux (Wells & Wettlaufer)

Which gives

$$w = \gamma \frac{\beta g \Pi}{\nu} [S_{br}(z_c) - S_0] \frac{z - z_c}{h - z_c}$$

# One-Dimensional Model of Convecting Sea Ice



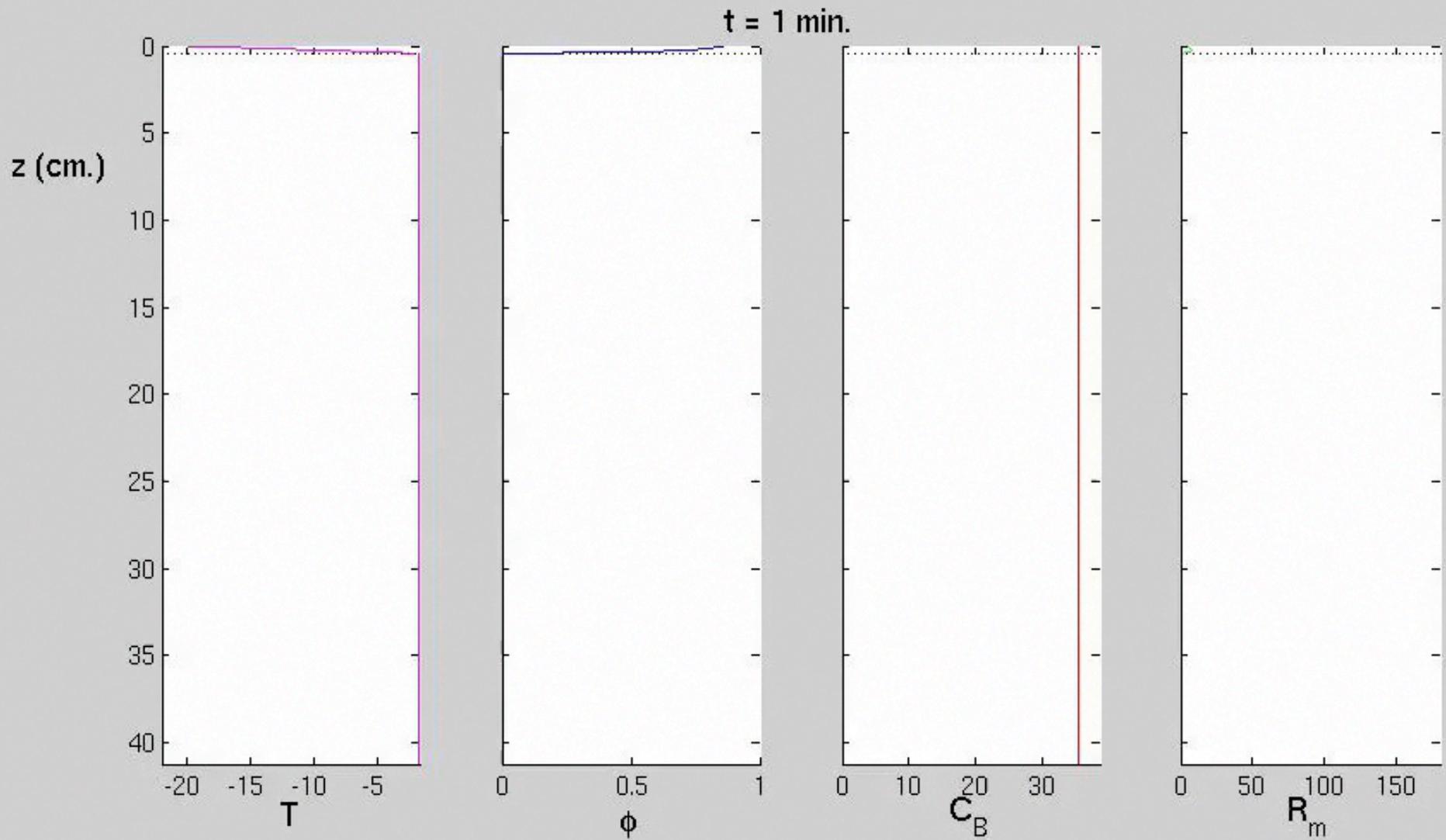
Depth of convecting region set by critical Rayleigh number

$$\frac{\beta g [C(z_c) - C_0] \langle \Pi \rangle h}{\kappa \nu} = R_c$$

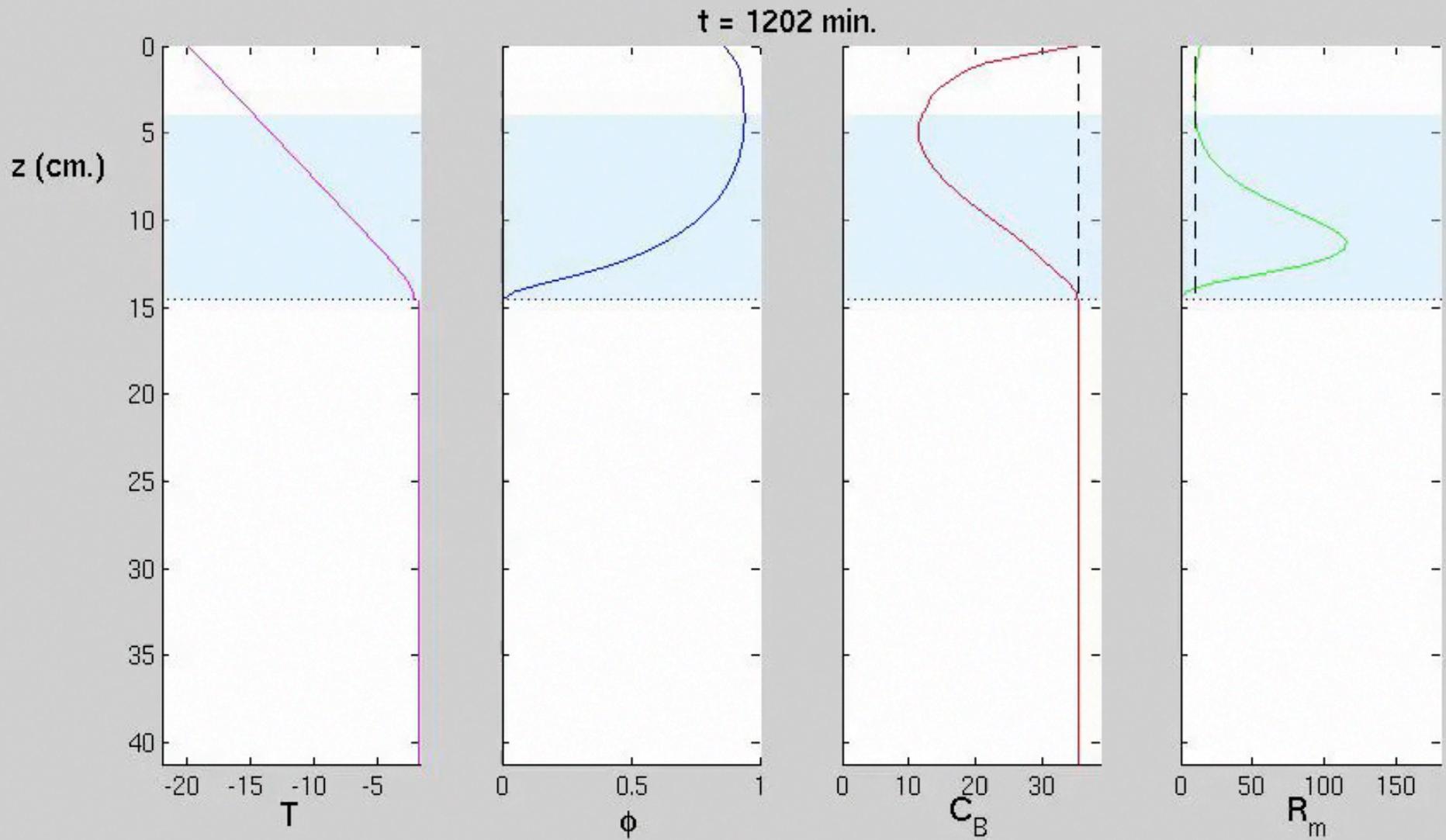
One-dimensional modelling of convecting mushy layer

$$c \frac{\partial T}{\partial t} + \rho_{br} c_{br} w \frac{\partial T}{\partial z} = \nabla \cdot (k \nabla T)$$

# Evolution of Convecting Sea Ice



# Evolution of Convecting Sea Ice



# Capabilities and Characteristics of 1-D Convection Schemes

Buoyancy flux determined dynamically – not thermodynamically tied to growth rate.

Capture delay in onset of convection seen in some experiments.

Predict enhancement or re-initiation of brine drainage during periods of warming.

Straightforwardly adjust to different ocean salinities.

# Summary

Convection begins at a critical value of the Rayleigh number

Convective fluxes (eg brine fluxes) are best parameterized in terms of a Rayleigh number

The Rayleigh number for a mushy layer (sea ice) depends on permeability and solutal buoyancy but thermal diffusivity

Convection in sea ice causes formation of brine channels by dissolution

Convection in a mushy layer is confined to a region near the ice–ocean interface.